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<http://dx.doi.org/10.1016/j.clinbiomech.2015.09.012>

<b>Title</b>	Technique determinants of knee joint loads during pivoting in female soccer players
<b>Authors</b>	Jones, PA, Herrington, LC and Graham-Smith, P
<b>Publication title</b>	Clinical Biomechanics
<b>Publisher</b>	Elsevier
<b>Type</b>	Article
<b>USIR URL</b>	This version is available at: <a href="http://usir.salford.ac.uk/id/eprint/37862/">http://usir.salford.ac.uk/id/eprint/37862/</a>
<b>Published Date</b>	2016

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# **TECHNIQUE DETERMINANTS OF KNEE ABDUCTION MOMENTS DURING PIVOTING IN FEMALE SOCCER PLAYERS.**

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**Abstract: 202 words**

**Word Count: 4168 words**

1 **ABSTRACT**

2 *Background:* No previous studies have investigated the optimal technique for pivoting with  
3 regard to reducing peak knee abduction moments and potential knee injury risk. The aim of  
4 this study was to investigate the relationships between technique characteristics and peak knee  
5 abduction moments during pivoting.

6 *Methods:* Twenty-seven female soccer players [mean (SD); age: 21 (3.8) years, height: 1.67  
7 (0.07) m, and mass: 60.0 (7.2) kg] participated in the study. Three dimensional motion  
8 analyses of pivots on the right leg were performed using 10 Qualysis 'Pro reflex' infrared  
9 cameras (240Hz). Ground reaction forces were collected from two AMTI force platforms  
10 (1200Hz) embedded into the running track to examine penultimate and final contact.  
11 Pearson's correlation coefficients, co-efficients of determination and stepwise multiple  
12 regression were used to explore relationships between a range of technique parameters and  
13 peak knee abduction moments. Significance was set at  $P < 0.05$ .

14 *Findings:* Stepwise multiple regression found that initial foot progression and initial knee  
15 abduction angles together could explain 35% (30% adjusted) of the variation in peak knee  
16 abduction moments ( $F_{(2,26)} = 6.499, P=0.006$ ).

17 *Interpretation:* The results of the present study suggest that initial- foot progression and knee  
18 abduction angles are potential technique factors to lower knee abduction moments during  
19 pivoting.

20 **Keywords:** Anterior Cruciate Ligament; Injury; Knee Abduction Moment; Technique; 180°  
21 Turns

22

23

24

## 25 1.0 INTRODUCTION

26 Cutting and pivoting have been identified as key actions associated with non-contact  
27 anterior cruciate ligament (ACL) injuries in female athletes (Boden, Dean, Feagin & Garrett,  
28 2000; Olsen, Myklebust, Engebretsen & Bahr, 2004; Faude, Junge, Kindermann & Dvorak  
29 2005), as such actions involve lower limb postures that increase knee abduction moments  
30 (Cortes *et al.*, 2011), which could lead to increased ACL strain (Shin, Chaudhari, &  
31 Andriacchi, 2009; Shin, Chaudhari, & Andriacchi, 2011) and subsequent injury. Several  
32 studies have investigated optimal cutting technique for reducing knee abduction moments and  
33 knee injury risk (McLean, Huang & van der Bogert, 2005; Sigward & Powers, 2007;  
34 Dempsey, Lloyd, Elliot, Steele, Munro & Russo, 2007; Dempsey, Lloyd, Elliot, Steele &  
35 Munro, 2009; Jamison, Pan & Chaudhari, 2012; Kristianlunds, Faul, Bahr, Myklebust &  
36 Krosshaug, 2014; Havens & Sigward, 2015; Jones, Herrington & Graham-Smith, 2015),  
37 whilst no previous studies have examined pivoting or 180° turns in this regard.

38 Previous research into cutting has revealed that the magnitude of lateral leg plant  
39 (Dempsey *et al.*, 2007; Dempsey *et al.*, 2009; Havens & Sigward, 2015; Jones *et al.*, 2015),  
40 lateral trunk flexion (Dempsey *et al.*, 2007; Dempsey *et al.*, 2009; Jamison *et al.*, 2012; Jones  
41 *et al.*, 2015) and initial knee abduction angles (McLean *et al.*, 2005; Kristianlunds *et al.*, 2014;  
42 Jones *et al.*, 2015) are influential in determining the magnitude of peak knee abduction  
43 moments. McLean *et al.* (2005) examined initial lower limb postures in 10 male and 10  
44 female NCAA athletes performing 45° side-step cuts and found greater peak knee abduction  
45 moments were associated with larger initial hip flexion, internal rotation and knee abduction  
46 angles, with knee abduction moments more sensitive to the later 2 variables in females. In  
47 addition, Sigward and Powers (2007) found that lateral ground reaction forces (GRF), initial-  
48 foot progression, hip rotation and abduction angles could explain 49% of the variation in peak  
49 knee abduction moments during 45° cutting in female soccer players. Such technique aspects

50 are a likely result of performance demands. For example, a wide lateral foot placement during  
51 cutting is necessary to generate medial GRF to facilitate the direction change.

52 As mentioned previously, a limitation of previous studies into optimal cutting  
53 technique for injury prevention is that with the exception of a few (Kristianlunds et al., 2014;  
54 Havens & Sigward, 2015; Jones et al., 2015), the majority of studies have only considered  
55 cutting between the angles of 30 to 60°, whilst none have examined pivoting (180°).  
56 Notational analysis in male Premier league soccer has shown that changing direction  
57 manoeuvres involving greater angles of direction change (90 to 180°) (Bloomfield, Polman &  
58 O'Donoghue, 2007) can frequently occur, and these may exacerbate knee joint loads. Cortes  
59 et al. (2011) found that pivoting significantly increases knee abduction motion and moments  
60 [-12.2 (7.0)° / 0.72 (0.3) N.m/kg.m] compared to drop jump landings [-3.9 (8.0)°/ 0.14 (0.07)  
61 N.m/kg.m] and 45° cutting [-3.8 (10)°/ 0.17 (0.5) N.m/kg.m] in female soccer players. This is  
62 perhaps due to the different task demands, with the need to decelerate to a complete stop  
63 before accelerating again during the pivot compared to laterally planting the leg and shifting  
64 momentum to the opposite side during a 45° cut.

65 Because of the different task demands between cutting and pivoting many of the  
66 parameters previously found with regard to optimal cutting technique may not necessarily be  
67 associated with peak knee abduction moments during pivoting. However, some of the  
68 variables identified previously such as initial knee abduction (McLean et al., 2005;  
69 Kristianlunds et al., 2014; Jones et al., 2015), hip internal rotation angles (McLean et al.,  
70 2005; Sigward and Powers, 2007; Havens & Sigward, 2015) and lateral trunk flexion  
71 (Dempsey et al., 2007; Dempsey et al., 2009; Jamison et al., 2012; Jones et al., 2015) might  
72 be expected to be associated with peak knee abduction moments during pivoting. Increased  
73 initial hip internal rotation angles leads to a more medially placed knee (i.e., greater initial  
74 knee abduction angle) relative to the GRF vector, resulting in an increased moment arm that

75 would elevate knee abduction moments during changing direction tasks (Sigward & Powers,  
76 2007). Whereas trunk position during landing and changing direction manoeuvres is often a  
77 critical factor in influencing knee joint loads (Mendiguchia et al., 2011) as the trunk is the  
78 largest segment of the body and thus, influences the position of the GRF vector relative to the  
79 knee joint during such manoeuvres. Therefore, initial knee abduction, hip rotation, and  
80 sagittal and frontal plane trunk flexion may influence knee abduction moments during  
81 pivoting and thus, should be considered in developing a model of technique for this  
82 manoeuvre.

83 Previous research (Cortes et al., 2011) has suggested that increased initial foot  
84 progression angle away from the direction of travel may account for the high knee abduction  
85 moments observed during pivoting. An increased initial foot progression angle or a more  
86 rotated pelvis during pivoting would be an attempt by athletes to facilitate the direction  
87 change by reducing the amount of rotation required during final contact (the phase when a  
88 subject makes contact with the ground and initiates movement into a different direction) and  
89 then re-acceleration. However, greater initial foot progression angle (or pelvic rotation) would  
90 lead to athletes absorbing the large impact forces at final contact through the frontal plane  
91 potentially increasing knee abduction moments, whereas reducing this angle would allow the  
92 large forces to be absorbed through the sagittal plane utilising the large knee and hip extensor  
93 muscle groups (e.g., peak external knee and hip flexor moments). Furthermore, if the thigh is  
94 more abducted or the foot is planted a large distance from the pelvis (i.e., greater last step  
95 length or horizontal distance between pelvis and foot) with an increased foot progression  
96 angle may further increase the moment arm of the GRF vector relative to the knee joint  
97 (similar to the effect of increased lateral leg plant during cutting) and thus increase peak knee  
98 abduction moments. Therefore, research into developing an optimal technique for pivoting  
99 should investigate these variables to confirm such a hypothesis.

100 Pivoting requires athletes to decelerate their velocity to zero, before reaccelerating in  
101 the opposite direction, whereas cutting involves shifting momentum into a different direction.  
102 Therefore, the deceleration strategy during pivoting may be influential in lowering forces  
103 during final contact and subsequently knee abduction moments. Graham-Smith, Atkinson,  
104 Barlow and Jones (2009) have found that penultimate contact (2<sup>nd</sup> to last foot contact with the  
105 ground during a pivot before moving into a new intended direction) prior to the turn resulted  
106 in greater vertical and anterior-posterior GRF's and internal knee extensor moments compared  
107 to final contact during a pivot in male soccer players. Thus, analysis of penultimate contact  
108 may provide more insight into the optimal technique for pivoting for reduced knee injury risk.  
109 Theoretically, if the majority of forward momentum can be reduced during penultimate  
110 contact, then lower external knee abduction moments may be experienced during the turn,  
111 where injuries often occur (Boden et al., 2000; Olsen et al., 2004) due to lower resultant  
112 GRF's. If the deceleration strategy is emphasised towards final contact this will increase  
113 resultant GRF at final contact which could increase peak knee abduction moments (Graham-  
114 Smith et al., 2009; Jones et al., 2015). Research should perhaps consider the deceleration  
115 strategy between penultimate and final contacts by examining a final / penultimate contact  
116 peak horizontal GRF ratio (HGRFR). Thus, if greater horizontal force can be generated during  
117 the penultimate contact relative to the final contact (i.e., a lower ratio) this may indicate  
118 greater braking during the penultimate contact which may lower resultant GRF and  
119 subsequent peak knee abduction moments during final contact.

120 The aim of this study was to investigate the relationships between technique  
121 characteristics and peak knee abduction moments during pivoting. The study investigates  
122 whether HGRFR, sagittal plane hip and knee joint moments and a number of initial lower  
123 limb, pelvis and trunk positions are associated with peak knee abduction moments. It is  
124 hypothesised that these variables are related to peak knee abduction moments during pivoting.

125

## 126 **2.0 METHODS**

### 127 **2.1 SUBJECTS**

128 Twenty-seven female soccer players [mean (SD); age: 21 (3.8) years, height: 1.67  
129 (0.07) m, and mass: 60.0 (7.2) kg] acted as subjects for the study. All players were registered  
130 with Soccer clubs playing in the second tier of English Women's Soccer. Written informed  
131 consent was attained from all subjects and approval for the study was provided by the  
132 University's ethical committee.

133

### 134 **2.2 RESEARCH DESIGN**

135 Testing took place on an indoor Mondo running surface. Each subject was required to  
136 attend the lab on 2 separate occasions. The first occasion was a familiarization session on the  
137 protocols used in the study with data collected on the subsequent session. The pivot involved  
138 the subjects running towards 2 force platforms. The first force platform was used to measure  
139 GRFs from the penultimate (left) foot contact, whilst the 2<sup>nd</sup> force platform was used to  
140 measure GRFs from the final (right) foot contact. Prior to the turn the subject ran through, a  
141 set of timing lights 5 m from the centre of the last platform. The subjects then turned (180°)  
142 back to the original starting position once contacting the end force platform with the right leg.  
143 Total time to complete the task was measured using a set of Brower timing lights (Draper,  
144 UT). The timing lights were set at approximate hip height for all subjects as previously  
145 recommended (Yeadon, Kato & Kerwin, 1999), to ensure that only one body part (i.e., lower  
146 torso) breaks the beam. Task completion time was used to monitor performance between trials  
147 and subjects. During familiarization and practice trials subjects were given feedback to  
148 regulate the time to complete the task, so that they could gage the speed of approach they used  
149 during subsequent data collection. Each subject started approximately 5 metres behind the



150 first set of timing lights. Some flexibility was allowed for the exact starting point for each  
151 subject to allow for the subjects differing stride pattern as they approached the end 2 force  
152 platforms. Each subject was allowed time prior to data collection to identify their exact  
153 starting point to ensure appropriate force platform contacts.

154         During data collection all subjects performed a minimum of 6 ‘Good’ trials of the  
155 pivot task. A good trial was considered to involve; 1) a straight approach to the force plates  
156 without prior stuttering or prematurely turning prior to final contact, 2) contact with the first  
157 force platform during penultimate (left) foot contact 3) contact with the central portion of the  
158 last platform during final contact to ensure a homogeneous distance of travel between trials  
159 and 4) recording an appropriate time to complete the task [2.65 s (10%)]. Trials were  
160 subsequently disqualified if the subject did not adhere to these characteristics. Verbal  
161 feedback was provided to rectify any of the abovementioned aspects on subsequent trials. The  
162 turn times were selected based on pilot work and used to control for performance of the tasks  
163 within and between subjects. In addition, for each trial the horizontal velocity in the direction  
164 of motion of the right hip joint centre was calculated over the 10 frames prior to penultimate  
165 foot contact to determine approach velocity in accordance with McLean et al. (2005). This  
166 retrospective analysis was conducted to ensure that each subjects trial achieved a target  
167 approach velocity of between 3.6 to 4.4 m·s<sup>-1</sup> for the pivot task. These target approach  
168 velocities were selected based on velocities recorded in several previous studies (McLean et  
169 al., 2005; Cotes et al., 2011) and previous pilot data collected in this lab.

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## 175 **2.3 PROCEDURES**

176 The procedures have been reported previously (Jones *et al.*, 2014; Jones *et al.*, 2015).  
177 Thus, only a brief overview is provided here. Reflective markers (14 mm spheres) were  
178 placed on body landmarks (see Jones *et al.*, 2014) of each subject by the same researcher to  
179 ensure marker placement consistency. Subjects wore ‘cluster sets’ (4 reflective markers  
180 attached to a light weight rigid plastic shell) attached using Velcro elasticated wraps on the  
181 right and left thigh and shin to approximate the motion of these segments during dynamic  
182 trials. The pelvis and trunk cluster sets were attached using an elasticated belt and Lycra ‘crop  
183 top’, respectively.

184 Three dimensional motions of these markers were collected whilst performing the  
185 pivots using 10 Qualysis ‘Pro reflex’ (Model no. MCU 240) infrared cameras (240Hz)  
186 operating through Qualysis Track Manager software (version 1.10.282). GRFs were collected  
187 from two AMTI (Model no. 600900) force platforms (1200Hz) embedded into the running  
188 track. The force platform arrangement allowed data to be collected for both the final and  
189 penultimate contact.

190 From a standing trial, a 6-degree-of-freedom model of the lower extremity and trunk  
191 was created for each participant, including trunk, pelvis, thigh, shank and foot using Visual  
192 3D software (C-motion, version 3.90.21). This kinematic model was used to quantify the  
193 motion at the hip, knee and ankle joints using Cardan angle sequence (Grood & Suntay,  
194 1983). The local coordinate system was defined at the proximal joint centre for each segment.  
195 The static trial position was designated as the subject’s neutral (anatomical zero) alignment,  
196 and subsequent kinematic measures were related back to this position. Lower limb joint  
197 moments were calculated using an inverse dynamics approach (Winter, 1990) through  
198 Visual3d software (C-motion, version 3.90.21) and are defined as external moments.  
199 Segmental inertial characteristics were estimated for each participant (Dempster, 1955). The

200 model utilised a CODA pelvis orientation (Bell, Brand & Pedersen, 1989) to define the  
201 location of the hip joint centre. The knee and ankle joint centres were defined as the mid-point  
202 of the line between lateral and medial markers. A minimum of 4 trials were used in the  
203 analysis of each subject based on visual inspection of the motion files. Trials were  
204 disqualified if approach velocity fell outside of the desired ranges stated above or if the  
205 subjects slid, turned prematurely or missed the force platform that went unnoticed during data  
206 collection. The trials were time normalised for each subject, with respect to the ground contact  
207 time of the pivot. Initial contact was defined as the instant after ground contact that the  
208 vertical GRF (vGRF) was higher than 20 N and end of contact was defined as the point where  
209 the vGRF subsided past 20 N for both penultimate and final contacts. The weight acceptance  
210 phase of ground contact was defined as from the instant of initial contact (vGRF > 20N) to the  
211 point of maximum knee flexion during ground contact as used previously (Havens &  
212 Sigward; 2015; Jones *et al.*, 2015). Joint coordinate and force data were smoothed in visual  
213 3D with a Butterworth low pass digital filter with cut-off frequencies of 12Hz and 25Hz,  
214 respectively. Cut off frequencies were selected based on a residual analysis (Winter, 1990)  
215 and visual inspection of the data.

216       During final contact of the pivot task the following angles were determined at the  
217 point of initial contact; foot progression (angle of foot orientation relative to the original  
218 direction of travel [0° straight, positive rotated inward (anti-clockwise), negative rotated  
219 outward (clockwise)], pelvic rotation (angle of the pelvis in the transverse plane relative to the  
220 original direction of travel at initial contact [0° neutral pelvis position, positive anticlockwise  
221 rotation]), knee abduction (positive adduction/ negative abduction), hip abduction (positive  
222 adduction/ negative abduction) and rotation (positive internal rotation/ negative external  
223 rotation), hip, knee, and ankle in the sagittal plane, trunk flexion relative to a vertical line  
224 perpendicular to the pelvis (0° upright, positive trunk lean forward, negative trunk leaning

225 back) and lateral trunk flexion relative to a vertical line perpendicular to the pelvis (0°  
226 upright, positive trunk lean away from the planted leg, negative trunk leaning towards the  
227 planted leg). Touchdown distance (horizontal distance from the centre of mass of the pelvis  
228 to centre of mass of the right foot at initial contact using the global co-ordinate system) and  
229 last step length (horizontal distance from the centre of mass of the left foot at penultimate  
230 contact to the right foot at final contact using the global co-ordinate system), sagittal plane  
231 peak knee and hip flexor moments during final contact were also determined. To evaluate  
232 deceleration strategy from penultimate to final contact and its relationship to peak knee  
233 abduction moments during final contact, a final/ penultimate contact horizontal (Fx  
234 component) GRF ratio (HGRFR) was also calculated.

235

## 236 **2.4 STATISTICAL ANALYSIS**

237

238 All statistical analysis was performed in SPSS for windows v17 (Chicago, Ill).  
239 Normality for each variable was examined using a Shapiro-Wilks test. Pearson's correlation  
240 coefficients, co-efficients of determination ( $R^2 \times 100\%$ ) and stepwise multiple regression  
241 were used to explore relationships of the abovementioned variables and peak knee abduction  
242 moments. For the stepwise multiple regression only significantly correlated variables were  
243 considered. Significance was set at  $P < 0.05$ .

244

## 245 **3.0 RESULTS**

246 Descriptives for each variable can be found in Table 1. Mean (SD) approach velocity  
247 and total times to the complete the task were  $4.02 (0.2) \text{ m}\cdot\text{s}^{-1}$  and  $2.67 (0.11) \text{ s}$ , respectively.  
248 Only initial foot progression (Figure 2b), initial knee abduction angles (Figure 2a) and peak  
249 hip flexor moments were significantly ( $p < 0.05$ ) correlated to peak knee abduction moments

250 (Table 1) during final contact. Stepwise multiple regression analysis found that initial foot  
251 progression angle and initial knee abduction angle together could explain 35% (30% adjusted)  
252 of the variation in peak knee abduction moments ( $F_{(2,26)} = 6.499$ ,  $P=0.006$ ). The regression  
253 equation is summarised in Table 2.

254

#### 255 **4.0 DISCUSSION**

256 The aim of the present study was to investigate the relationships between pre-  
257 determined technique characteristics and peak knee abduction moments during pivoting.  
258 Initial foot progression and knee abduction angles were the main predictors of peak knee  
259 abduction moments (35%) during pivoting, providing support for these variables in the a-  
260 priori theory.

261 Previous research (McLean *et al.*, 2005; Sigward & Powers, 2007; Dempsey *et al.*,  
262 2007; Dempsey *et al.*, 2009), have attempted to evaluate technique characteristics responsible  
263 for increasing peak knee abduction moments during 30 to 60° cutting, which may not truly  
264 represent the changing direction demands of soccer (Bloomfield *et al.*, 2007; Greig, 2009). No  
265 previous research has examined pivoting with regard to technique determinants of peak knee  
266 abduction moments. In the present study, only initial knee abduction and foot progression  
267 angles were found to be related to peak knee abduction moments, explaining 35% (30%  
268 adjusted) of the variation. Cortes *et al.* (2011) previously suggested that increased (inward)  
269 foot progression angle may be a key variable that could influence knee joint loads during  
270 pivoting, but presented no data to support this. Reducing the initial foot progression angle to a  
271 close to straight foot position, has the effect of allowing the large forces to be absorbed  
272 through the sagittal plane utilising the large knee and hip extensor muscle groups to fully  
273 absorb the GRF generated. In support of this, a significant correlation was observed between  
274 peak hip flexor moments and peak knee abduction moments ( $R = -0.388$ ,  $R^2 = 15\%$ ,  $P < 0.05$ ).

275 The greater the peak hip flexor moments produced during final contact the lower the peak  
276 knee abduction moments. Whereas a more rotated foot during weight acceptance creates an  
277 external knee abduction moment, as the force vector is lateral to the knee joint. It should be  
278 noted however, that in order to then execute the turn from a straighter initial foot position, the  
279 athlete should unload to allow the foot to rotate and avoid generating large rotational stress at  
280 the shoe-surface interface.

281 Increased initial knee abduction angle was also found to be significantly related to  
282 peak knee abduction moments and has previously been found for cutting (McLean *et al.*,  
283 2005; Kristianlunds *et al.*, 2014; Jones *et al.*, 2015). Greater initial knee abduction angles  
284 have the effect of shifting the knee more medial relative to the GRF vector. This in turn leads  
285 to a greater moment arm between the knee joint axis and GRF vector and consequently  
286 greater knee abduction moments. Therefore, as with cutting it is recommended that during  
287 pivoting, athletes avoid or limit the amount of knee abduction during early ground contact to  
288 lower knee abduction moments.

289 Increased maximal horizontal braking forces [-1.79 (0.29) BW] during the penultimate  
290 contact relative to the final contact [-1.65 (0.29) BW] were observed; substantiating our  
291 earlier research on pivoting in male soccer players (Graham-Smith *et al.*, 2009) and 90°  
292 cutting in female soccer players (Jones *et al.*, 2015). Theoretically, this deceleration strategy  
293 has the advantage of reducing the resultant GRF during final contact, which would influence  
294 external knee joint loads during final contact. When considering the HGRFR for both  
295 manoeuvres no relationship was observed with peak knee abduction moments. However, on  
296 further analysis players with greater (n = 9) peak knee abduction moments (+0.5 SD) had a  
297 higher ratio than players exhibiting lower (n = 8) peak knee abduction moments (-0.5 SD)  
298 [0.99 (0.24) vs. 0.92 (0.18)]; similar to our earlier research on 90° cutting (Jones *et al.*, 2015)  
299 and suggests that players with lower peak knee abduction moments do so by braking more

300 during penultimate contact. Therefore, the lack of a relationship found may be due to the low  
301 sample size in the present study. Future studies should perhaps consider a more in-depth  
302 kinetic and kinematic evaluation of the penultimate contact in order to gather a greater  
303 understanding of the role of penultimate contact during pivoting and potentially develop a  
304 more comprehensive model of optimal technique for the manoeuvre.

305 A limitation of the present study is the pre-planned execution of the pivot task as  
306 opposed to unanticipated, which has been used in previous studies (Besier, Lloyd, Cochrane  
307 & Ackland, 2001; Cortes *et al.*, 2011) and shown to elevate knee joint loads during cutting  
308 (Besier *et al.*, 2001). Future studies need to confirm the technique factors identified in the  
309 present study under unanticipated conditions.

310 Another limitation of the present study, is that the model developed only included 2  
311 variables and explained 35% of the variance in peak knee abduction moments, thus, perhaps  
312 limits the application of these findings in developing a model of optimal technique for  
313 pivoting to reduce injury risk. This may be due to the generally low sample size used in the  
314 present study (n=27), which limits the number of variables that can be integrated into the  
315 model (Vincent, 1995). For instance, a greater sample size may have led to the inclusion of  
316 the significantly correlated peak hip flexor moments into the model. Furthermore, it is  
317 possible that additional variables have been missed by the authors in the a-priori theory. As  
318 mentioned above, some further kinematic and kinetic variables from penultimate contact may  
319 be associated with peak knee abduction moments during final contact. Thus, further research  
320 particularly of penultimate contact is needed to develop this model further in order to identify  
321 a definitive model of technique for pivoting with regard to injury prevention.

322 Previous research into 45 – 90° cutting in males and females have found associations  
323 between peak knee abduction moments and initial hip internal rotation (Sigward & Powers,  
324 2007; Havens & Sigward, 2015), hip abduction (Sigward & Powers, 2007), lateral trunk

325 flexion (Dempsey et al., 2007, Jamison et al., 2012; Jones et al., 2015), hip flexion (McLean  
326 et al., 2005) and peak internal knee extensor moments (Havens & Sigward, 2015). Therefore,  
327 it was expected that these variables may be related to peak knee abduction moments during  
328 pivoting. With many of these variables showing no or weak correlations ( $R \leq 0.3$ ) it is  
329 unlikely that they are related to peak knee abduction moments during pivoting. Although low,  
330 both initial pelvis and hip internal rotation angles revealed correlations greater than 0.3 with  
331 the later close to significance ( $P = 0.07$ ) and are thus, worth considering in future  
332 investigations with greater sample sizes to develop a model of technique for pivoting.

333 Finally, due to the need to control for performance aspects (i.e., turn times, approach  
334 velocity) between subjects it was beyond the scope of the study to evaluate what technique  
335 aspects influence performance and whether such aspects would contradict the findings from  
336 the present study for reducing peak knee abduction moments. For example, an increased foot  
337 progression angle might be beneficial for reducing total time to complete the task, as this  
338 would help rotate more of the body prior to final foot contact but has the negative effect of  
339 increasing peak knee abduction moments. Future research should examine this conflict  
340 between performance requirements and injury risk during changing direction tasks in more  
341 detail by examining what technique parameters are associated with total time to complete the  
342 pivot task used in the present study (i.e., subjects aim to complete the task as fast as possible  
343 without controlling for approach velocity and performance time) and whether these  
344 parameters are also associated with large peak knee abduction moments. Without recognising  
345 the implications for performance in research, limits the application of any findings related to  
346 injury prevention through technique interventions during agility training methods, as players  
347 and coaches are more likely to adhere to training programmes with a performance centred  
348 focus.

349



350 **5.0 CONCLUSION**

351           The aim of the present study was to investigate the relationships between technique/  
352 biomechanical characteristics and peak knee abduction moments during pivoting. Initial foot  
353 progression and knee abduction angles were identified as significant technique predictors of  
354 peak knee abduction moments during pivoting. These findings reveal potential technique  
355 factors to develop a model for pivoting technique for injury prevention purposes.

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357 **ACKNOWLEDGEMENTS**

358 *No funding was received to support this study. The authors have no conflict of interest.*

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445 **FIGURE AND TABLE LEGENDS**

446 Figure 1. Plan view of the experimental set-up.

447 Figure 2. Scatter plots for the relationships between initial knee abduction angle (2a) and  
448 initial foot progression angle (2b) with peak knee abduction moments.

449 Table 1. Mean (SD) technique variables and the relationships to peak knee abduction  
450 moments during pivoting.

451 Table 2. Stepwise multiple regression of predictors of peak knee abduction moments during  
452 pivoting.

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459 **TABLE 1**

Variable	Mean (SD)	Relationships to knee abduction moments	
		R	R <sup>2</sup>
Knee Abduction Moments (Nm.kg <sup>-1</sup> ) during weight acceptance of final contact	1.24 (0.41)		
Initial Foot Progression Angle at final contact (°)	18 (18.4)	0.49*	24%
Initial Pelvis Rotation Angle at final contact (°)	52 (14.1)	0.32	9.9%
Initial knee abduction angle at final contact (°)	-4 (4.9)	-0.49*	24%
Initial hip abduction angle at final contact (°)	-20 (6.9)	0.06	>1%
Initial hip rotation angle at final contact (°)	14 (9.1)	-0.35	12.3%
Initial Trunk Flexion Angle (°)	18 (9.5)	-0.26	6.9%
Initial Lateral Trunk Flexion Angle (°)	-1.9 (5.8)	0.20	3.8%
Initial Hip Flexion Angle (°)	45 (13.5)	-0.1	1%
Initial Knee Flexion Angle (°)	24 (6.3)	-0.03	<1%

Initial Ankle Angle (°)	58 (11.6)	-0.04	<1%
Last step length (m)	0.79 (0.07)	0.18	3.1%
Horizontal touchdown distance (m)	0.66 (0.04)	0.02	<1%
Peak Horizontal Braking Force Ratio	0.94 (0.19)	0.19	3.5%
Peak hip flexor moments (Nm·kg <sup>-1</sup> )	2.54 (0.69)	-0.39**	15%
Peak knee flexor moments (Nm·kg <sup>-1</sup> )	2.07 (0.34)	-0.17	3%

460 \*p = 0.01

461 \*\*p < 0.05

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464 **TABLE 2**

Blocks	B	Standard errors β	β
Block 1: Initial Knee Abduction Angle	-0.03	0.015	-0.363*
Block 2: Initial Foot Progression Angle	0.008	0.004	0.362*

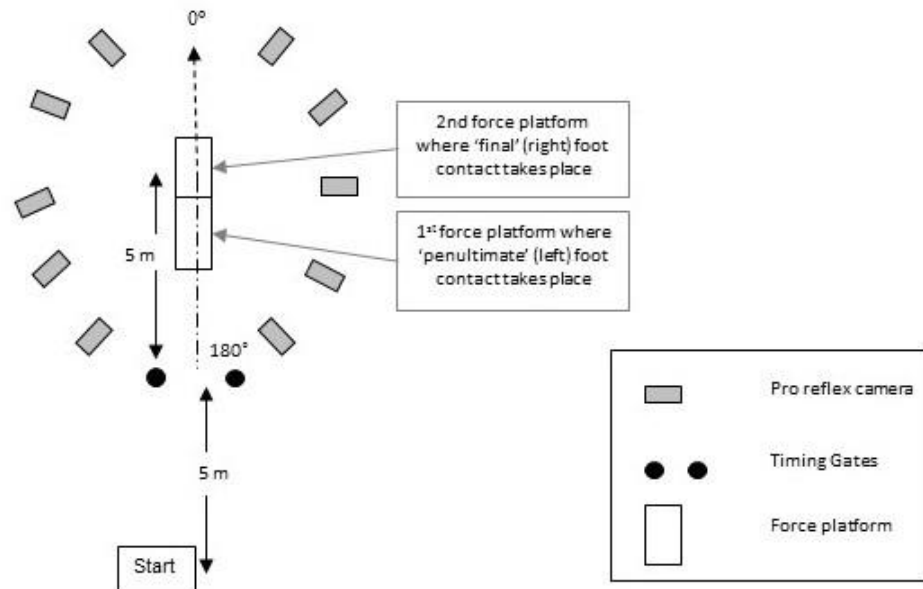
465 \*p<0.05

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**FIGURE 1**



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