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No differences in weightlifting overhead pressing exercises kinetics

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1 **No Differences in Weightlifting Overhead Pressing Exercises**
2 **Kinetics**

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4 Kinetics of the PP, PJ and SJ
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12 Soriano, M.A. Lake, J. Comfort, P. Suchomel, T.J. McMahon, J.J. Jiménez-Ormeño, E. & Sainz
13 de Baranda, P
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48 **Abstract**

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50 This study aimed to compare the kinetics between the push press (PP), push jerk (PJ), and
51 split jerk (SJ). Sixteen resistance-trained participants (12 men and 4 women; age: $23.8 \pm$
52 4.4 years; height: 1.7 ± 0.1 m; body mass: 75.7 ± 13.0 kg; weightlifting experience: 2.2
53 ± 1.3 years; one repetition maximum [1RM] PP: 76.5 ± 19.5 kg) performed 3 repetitions
54 each of the PP, PJ and SJ at a relative load of 80% 1RM PP on a force platform. The
55 kinetics (peak and mean force, peak and mean power, and impulse) of the PP, PJ and SJ
56 were determined during the dip and thrust phases. Dip and thrust displacement and
57 duration were also calculated for the three lifts. In addition, the inter-repetition reliability
58 of each variable across the three exercises was analyzed. Moderate to excellent reliability
59 was evident for the PP (Intraclass correlation coefficient [ICC] = 0.91 – 1.00), PJ (ICC =
60 0.86 – 1.00) and SJ (ICC = 0.55 – 0.99) kinetics. One-way analysis of variance revealed
61 no significant or meaningful differences ($p > 0.05$, $\eta^2 \leq 0.010$) for any kinetic measure
62 between the PP, PJ, and SJ. In conclusion, there were no differences in kinetics between
63 the PP, PJ, and SJ when performed at the same standardized load of 80% 1RM PP.

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66 **Key words:** push press, push jerk, split jerk, power output, biomechanics, force
67 platform.

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79 **Introduction**

80 Weightlifting exercises and their derivatives have been suggested to be effective
81 training tools to improve sports performance (Chiu & Schilling, 2005; Hori, Newton,
82 Nosaka, & Stone, 2005; Suchomel, Comfort, & Lake, 2017; Suchomel, Comfort, &
83 Stone, 2015). Researchers have highlighted that these exercises imitate sport-specific
84 movements by means of performing a forceful triple extension pattern of the hips, knees
85 and ankles (plantar flexion), while concurrently producing high rates of force
86 development and power (Comfort, Allen, & Graham-Smith, 2011a; Suchomel et al.,
87 2015). Moreover, researchers have shown that performance in weightlifting variations
88 such as the hang power clean is correlated with sprinting ($r = -0.58$, $p < 0.01$), jumping
89 ($r = 0.41$, $p < 0.05$) and change of direction performance ($r = -0.41$, $p < 0.05$) (Hori et al.,
90 2008). In addition, results of a recent meta-analysis revealed that training with
91 weightlifting exercises and their derivatives is more effective for increasing jumping
92 performance than employing traditional resistance training in resistance-trained
93 participants (~5% difference; effect size [ES] = 0.64, $p < 0.001$) (Hackett, Davies,
94 Soomro, & Halaki, 2016).

95 Researchers have demonstrated that exercise variation impacts one repetition
96 maximum (1RM) performance between weightlifting power clean and overhead pressing
97 exercises (Kelly, McMahon, & Comfort, 2015; Soriano et al., 2019). Similarly, the
98 kinetics can also be affected by weightlifting variations, with the majority of research in
99 this area focused on weightlifting pulling and catching derivatives (Comfort, Allen, &
100 Graham-Smith, 2011b; Suchomel et al., 2015; Suchomel, Wright, Kernozek, & Kline,
101 2014). For example, Comfort et al. (2011b) determined that peak force and power during
102 the mid-thigh power clean and mid-thigh clean pull were significantly greater ($p < 0.001$)
103 than equivalent data from the hang power clean (~19%, ~28%, respectively) and power

104 clean (~14%, ~12% difference, respectively). However, there were no significant
105 differences in the peak force, rate of force development and power between the mid-thigh
106 power clean and mid-thigh clean pull. Authors attributed these similarities in kinetics to
107 similar kinematics of the propulsion phase between lifts. Similarly, Suchomel et al.
108 (2014) found a significantly higher peak power output during the jump shrug compared
109 with hang clean (30%, $p < 0.001$) and high pull (19%, $p < 0.001$). Additionally, authors
110 reported significantly higher power outputs in the hang high pull when compared to the
111 hang power clean exercise (13%, $p < 0.001$). Altogether, these findings indicate that
112 exercise selection impacts the kinetics (e.g. force, power) of weightlifting pulling and
113 catching derivatives (Suchomel et al., 2017). However, while the kinetics of the
114 weightlifting pulling and catching derivatives have been studied extensively, little
115 information exists about the weightlifting overhead pressing derivatives.

116 Weightlifting overhead pressing exercises such as the push press (PP), push jerk
117 (PJ) and split jerk (SJ) are widely used by practitioners to enhance athlete ability to
118 generate high rates of force development and power (Comfort et al., 2016; Lake, Mundy,
119 & Comfort, 2014; Soriano, Suchomel, & Comfort, 2019). The PP, PJ and SJ have similar
120 lower-body movement pattern, which is comparable to a countermovement jump (CMJ)
121 and the propulsion phase of other weightlifting derivatives such as the hang power clean,
122 as previously established (Hori et al., 2008; Lake et al., 2014; Soriano et al., 2019). The
123 lifting strategy of the PP, PJ and SJ involve the dip and thrust phases. The dip is the
124 shallow squat which corresponds to the sum of the unweighing and braking phases
125 (similar to the CMJ), whereas the thrust is the rapid propulsion phase via extension of the
126 hips and knees, and plantar flexion of the ankles. It is during the thrust phase where the
127 highest rate of force development, barbell velocity and, consequently, power has been
128 recorded (Lake, Lauder, & Dyson, 2007; Lake et al., 2014). A strictly vertical movement,

129 and optimal duration and displacement during the dip and thrust phases are key aspects
130 of success in the PP, PJ, and SJ (Soriano et al., 2019). However, to the authors knowledge,
131 the differences in power, force or impulse during weightlifting overhead pressing
132 variations (PP, PJ or SJ) are not known and by studying these data we could help
133 practitioners make informed decisions about program design and weightlifting overhead
134 pressing exercises performance.

135 Therefore, the aim of this study was to compare the kinetics between the PP, PJ
136 and SJ exercises. Briefly, studying peak and mean force enables the coach to identify key
137 elements of the athlete's force generating capacity; power describes the rate at which
138 work is performed (based on the system centre of mass [COM]) (Lake, Lauder, & Smith,
139 2012; Turner et al., 2020); impulse explains the mean net force (force minus weight) and
140 duration of force application and is directly proportional to the subsequent momentum of
141 the mass of interest. It has been contested that because the impulse-momentum
142 relationship perfectly describes the requirements for "powerful" movements, strength and
143 conditioning coaches should focus on examining the underpinning components of net
144 impulse: net force and time (duration of force application) (Turner et al., 2020), therefore
145 propulsion phase duration will also be investigated. A further aim of this study was to
146 determine the inter-repetition reliability of each variable across the three exercises.
147 Reliability is important to be confident that any changes in performance are due to factors
148 other than errors associated with the test. In this case, determining within-session
149 reliability is important for quantifying the consistency of performance within the test
150 (Comfort, Jones, & McMahon, 2018). It was hypothesized that PP, PJ, and SJ dip and
151 thrust phase kinetics would not be different when performed with a standardized load,
152 because a similar lower-body lifting strategy (kinematics) will be used (Comfort,
153 McMahon, & Fletcher, 2013; Soriano et al., 2019).

154

155 **Methods**

156 *Participants*

157 Sixteen healthy resistance-trained participants, (12 men and 4 women; age: 23.8
158 \pm 4.4 years; height: 1.7 \pm 0.1 m; body mass: 75.7 \pm 13.0 kg; weightlifting training
159 experience: 2.2 \pm 1.3 years; 1RM PP: 76.5 \pm 19.5 kg) took part in this study. Participants
160 were competitors in CrossFit[®], rugby, volleyball, swimming, track and field, and
161 weightlifting (regional and national championships) and had \geq 6 months of weightlifting
162 experience. The PP, PJ and SJ were regularly performed (\geq 3 x a week) in their respective
163 strength and conditioning training preparation. There were no highly skilled weightlifters
164 in this study, with seven participants competing at regional and national level for at least
165 1 year. Participants were assessed by a certified strength and conditioning specialist
166 before the testing session to ensure that the exercises (PP, PJ and SJ) were performed
167 adequately. Participants were asked to replicate their fluid and food intake 24 hours before
168 each day of testing, to avoid strenuous exercise for 48 hours before testing, and to
169 maintain any existing supplementation regimen throughout the duration for the study. All
170 testing sessions were performed at the same time of day to minimize the effect of
171 circadian rhythms. The investigation was approved by the institutional review board of
172 the University, and all participants provided written informed consent before
173 participation. The study conformed to the principles of World Medical Association's
174 Declaration of Helsinki.

175

176 *Experimental design*

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178 A within-subjects repeated measures research design was used, whereby kinetics
179 (peak and mean force, peak and mean power, and impulse) were determined during the

180 PP, PJ and SJ. In addition, lower-body lifting strategy kinematics (dip and thrust
181 displacement and duration) were also calculated from the force-time data. The kinetics
182 were calculated from force platform derived data.

183

184 *Testing procedures*

185 Participants performed the one repetition maximum (1RM) single assessment
186 protocol during the PP defined by Soriano et al. (2019), which has previously reported a
187 high reliability and low variability in resistance-trained participants (ICC= 0.96; CV =
188 1.8%) (Soriano et al., 2019). The 1RM test was performed with a maximum of 7 days
189 before the biomechanics assessment. Subsequently, a standardized load of 80% of each
190 individual's previously determined 1RM PP was selected to perform all lifts to remove
191 the impact of load on the kinetics. This load has been identified as the optimal load for
192 maximal power production during the PP in previous research (Lake et al., 2014). The
193 barbell was lifted from squat stands before starting each attempt to minimize fatigue
194 associated with performance of the clean, which precedes the jerk in weightlifting
195 competitions.

196 For the biomechanics assessment, participants performed a standardized warm up
197 protocol previously described by Lake et al. (2014) and Soriano et al. (2019). This began
198 with 5 minutes of stationary running on a treadmill and continued with 2-3 minutes of
199 upper and lower-body dynamic stretching. The exercise-specific warm up part consisted
200 of one circuit of 10 repetitions of squats, front squats at $\frac{1}{4}$, $\frac{1}{2}$ and full depth, shoulder
201 press, PP, PJ and SJ, lifting the barbell mass only (20 kg). Subsequently, the specific
202 warm-up included one set of 5 submaximal (50-60% of the maximal perceived effort)
203 repetitions in each exercise (PP, PJ and SJ). Participants then rested for 5 minutes before
204 performing another set of 3 submaximal (70-75% of the maximal perceived effort)

205 repetitions in each exercise. After the warm-up, participants rested for 5 minutes before
206 biomechanics testing commenced as previously specified (Soriano et al., 2019).

207 During the biomechanics testing, exercise order was randomly assigned to each
208 participant so that they performed 1 set of 3 repetitions of each exercise, starting with
209 either the PP, PJ or the SJ. After each repetition, participants were instructed to put the
210 barbell back in the power rack and rest for 30 seconds to minimize fatigue, and ensure
211 technical proficiency and power maintenance during the PP, PJ and SJ (Comfort et al.,
212 2011b). The technical aspects of the exercises employed (PP, PJ and SJ) are well defined
213 in the literature and the guidelines previously provided were strictly followed to avoid
214 confusion and set appropriate technique standards (Lake et al., 2014; Soriano et al., 2019).
215 Briefly, in the PP the barbell must be pressed upward throughout the full extension of the
216 hips, knees, and ankles, flexion of the shoulders and extension of the elbows, while the
217 feet do not leave the ground. However, during the PJ participants fully extended the hip,
218 knee and ankle joints, accelerating the barbell upward before dropping under the barbell
219 in a ¼ squat, to catch the barbell with elbows and shoulders fully extended overhead. For
220 the SJ, participants followed the same initial instructions as in the PJ but instead of
221 catching the barbell in a ¼ squat, they split their feet fore and aft. Note that contrary to
222 the PP, the feet leave the ground for both the PJ and SJ.

223

224 *Measurement equipment and data analysis*

225 All tests were performed using standardized barbells and plates (Werksan weights
226 and Olympic bar; Werksan, Moorestown, New Jersey, USA), lifting platforms and power
227 racks (Powerlift, Iowa, USA). During the biomechanics testing, all lifts were performed
228 with participants standing on an in-ground force platform (AMTI, Advanced Medical
229 Technologies Inc, Newton, *Massachusetts*, USA) sampling at 1000 Hz, interfaced with a

230 laptop. Data were collected in Qualisys Trac Manager software and subsequently
231 analyzed using Excel (Microsoft, USA).

232 The kinetics (dip and thrust peak and mean force, power and impulse), as well as
233 the dip and thrust displacement and duration were derived from vertical force using the
234 methods previously described by Lake et al. (2014) and Soriano et al. (2020) during
235 weightlifting exercises. Data were analyzed using a customized Excel spreadsheet to
236 obtain the kinetics (mean and peak force, mean and peak power and impulse) and phase
237 duration and displacement. Velocity of the COM was obtained by subtracting barbell and
238 body weight (system weight: force averaged over 0.5 to 1.0 s period of pre-exercise
239 standing still) from vertical force to get net force before dividing it by system mass
240 (system weight / acceleration of gravity), and then integrating the product using the
241 trapezoid rule. Mechanical power achieved by displacing system mass was calculated as
242 the product of force and velocity of the COM (Soriano et al., 2020). Impulse was obtained
243 from the area under the net force-time curve during the dip and thrust phases using the
244 trapezoid rule (Lake et al., 2014). To describe the lower-body lifting strategy kinematics
245 underpinning the kinetics of these weightlifting variations (PP, PJ and SJ), COM
246 displacement and the duration of the dip and thrust phases were selected. The dip phase
247 began at the onset of the countermovement and ended at the velocity transition from
248 negative to positive (lowest system COM position). The onset of the countermovement
249 was identified as the instant when vertical force was reduced by a threshold equal to 5
250 times the standard deviation of the BW (calculated in the weighing phase), as previously
251 suggested (McMahon, Suchomel, Lake, & Comfort, 2018). The post-countermovement
252 transition from negative to positive velocity marked the beginning of the thrust phase
253 which ended at peak velocity, a point common to all three exercises that represents the
254 end of the positive displacement / positive acceleration part of the thrust phase (**Figure**

255 1). The dip corresponds to the sum of the unweighting and braking phases, whereas the
 256 thrust is the rapid propulsion phase via extension of the hips, knees and plantar flexion of
 257 the ankles (Soriano et al., 2019). Therefore, dip and thrust displacement were calculated
 258 by integrating the velocity-time curve with respect to time, and then phase durations were
 259 calculated (Flores et al., 2017; Lake et al., 2014). The repetition where the lifter achieved
 260 the highest power production during each weightlifting variation (PP, PJ and SJ), was
 261 selected for further analysis along with all dip and thrust kinetics (e.g. peak and mean
 262 force, peak and mean power and impulse) related to it, using Excel (Microsoft, USA).
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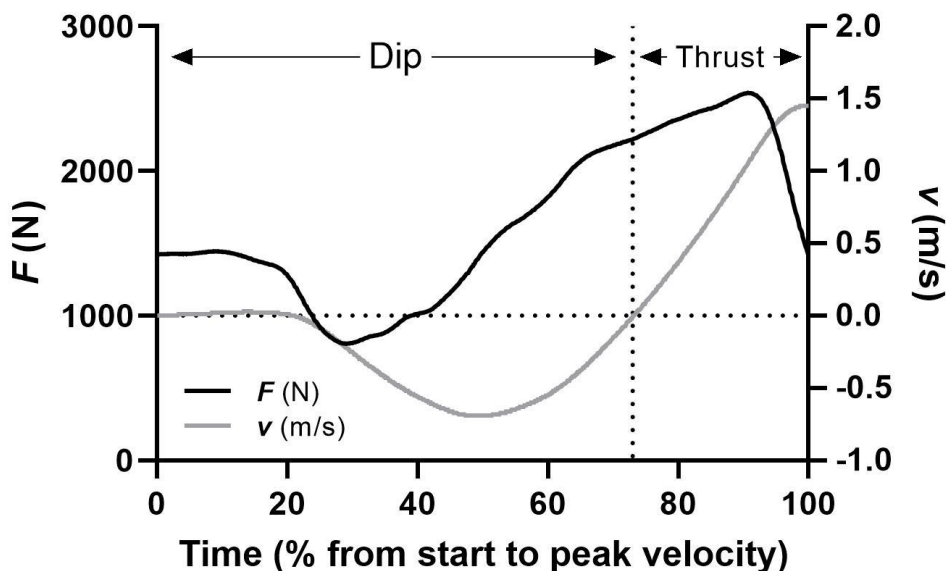


Figure 1. Graphic representation of the force-time and the integrated velocity-time characteristics of the push press exercise performed at 80% of 1RM by a random subject. Force is represented as the system mass (force exerted by the subject plus barbell and body weight). *F* force, *v* velocity. **Dip** corresponds to the unweighting and braking phases of the lift with negative direction. **Thrust** corresponds to the propulsion phase with positive direction.

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266 *Statistical Analyses*

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All data are presented as mean \pm SD, where appropriate. Inter-repetition reliability

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of the force-time characteristics for each exercise variation (PP, PJ and SJ) was

269 determined using the coefficient of variation (CV), intraclass correlation coefficient (ICC;
270 model 3.1) and associated 95% confidence intervals (CI). Intraclass correlation
271 coefficient and associated CI were interpreted based on the recommendations of Koo et
272 al. (2016) where values of the ICC lower bound $95\%CI \leq 0.50$ is indicative of poor
273 reliability, 0.5 and 0.74 indicate moderate reliability, 0.75 and 0.90 indicate good
274 reliability, and values > 0.90 indicate excellent reliability. A CV $< 10\%$ was used as a
275 criterion for the minimum acceptable reliability (Baumgartner & Chung, 2001). The
276 reliability analysis was performed by means of a custom spreadsheet (Hopkins, 2000).

277 After the assumption that data were normally distributed was confirmed using the
278 Shapiro-Wilk's test, a one-way analysis of variance (ANOVA) and Bonferroni post hoc
279 analysis were conducted to determine if there were any significant differences in force-
280 time characteristics between lifts. In addition, lifting strategy kinematics (dip and thrust
281 displacement and time) were also analyzed. An *a priori* alpha level was set at $p \leq 0.05$.
282 Eta squared (η^2) were used to determine the magnitude of the effect independently of the
283 sample size; η^2 has previously been recommended for ANOVA designs (Lakens, 2013),
284 and interpreted based on the recommendations of Cohen (Cohen, 1988) (small < 0.06 ,
285 medium = $0.06 - 0.14$ and large ≥ 0.14). All statistical analyses were performed using
286 SPSS version 25.0 for Mac (Chicago, IL, USA).

287 **Results**

288 Shapiro-Wilk test of normality revealed that all data were normally distributed (p
289 > 0.05). Intraclass correlation coefficients (and associated CI) revealed a high inter-
290 repetition reliability for all the kinetics (peak and mean force, peak and mean power, and
291 impulse) during the three exercises (PP, PJ, SJ) (**Table 1**). Briefly, reliability was good
292 to excellent for PP dip peak power, PJ dip peak force, dip peak power and dip mean
293 power. Compared to the PP and PJ, the SJ showed lower reliability. SJ dip peak force,

294 thrust mean force, dip peak power, thrust mean power and dip impulse reliability was
295 good to excellent; dip mean power reliability was moderate to good. Similarly, the low
296 %CV confirmed acceptable variability for most of the kinetics for the PP, PJ, and SJ
297 (**Table 1**). However, dip peak power during the PP (CV = 10.8%) and SJ (CV = 10.9%)
298 as well as dip mean power during the SJ (CV = 10.5%) exceeded the previously established
299 criterion of CV <10% for minimum acceptable reliability.

Table 1. Inter-repetition reliability of the kinetics during the push press, push jerk and split jerk exercises

Performance variables	Push press		Push jerk		Split jerk	
	ICC	%CV	ICC	%CV	ICC	%CV
Dip PF (N) (95% CI) [Interpretation]	0.97 (0.93 – 0.99) Excellent	3.00 (1.80 – 3.88) Acceptable	0.95 (0.89 – 0.98) Good	4.20 (3.39 – 5.86) Acceptable	0.93 (0.86 – 0.97) Good	2.69 (1.95 – 3.65) Acceptable
Thrust PF (N) (95% CI) [Interpretation]	0.98 (0.96 – 0.99) Excellent	2.69 (1.95 – 3.65) Acceptable	0.97 (0.94 – 0.99) Excellent	3.24 (2.81 – 4.61) Acceptable	0.97 (0.94 – 0.99) Excellent	2.85 (1.92 – 3.79) Acceptable
Dip MF (N) (95% CI) [Interpretation]	0.98 (0.95 – 0.99) Excellent	3.04 (1.89 – 3.97) Acceptable	0.97 (0.94 – 0.99) Excellent	3.23 (2.50 – 4.45) Acceptable	0.98 (0.96 – 0.99) Excellent	2.69 (1.95 – 3.65) Acceptable
Thrust MF (N) (95% CI) [Interpretation]	0.99 (0.98 – 1.00) Excellent	2.20 (1.41 – 2.89) Acceptable	0.98 (0.96 – 0.99) Excellent	2.42 (1.77 – 3.29) Acceptable	0.92 (0.85 – 0.97) Good	3.66 (5.92 – 6.57) Acceptable
Dip PP (W) (95% CI) [Interpretation]	0.93 (0.86 – 0.99) Good	10.84 (6.96 – 14.25) Unacceptable	0.94 (0.88 – 0.97) Good	8.10 (5.51 – 10.80) Acceptable	0.88 (0.77 – 0.95) Good	10.90 (5.21 – 13.46) Unacceptable
Thrust PP (W) (95% CI) [Interpretation]	0.98 (0.96 – 0.99) Excellent	5.44 (4.79 – 7.78) Acceptable	0.98 (0.97 – 0.99) Excellent	3.24 (1.39 – 3.93) Acceptable	0.96 (0.92 – 0.98) Excellent	4.29 (5.82 – 7.14) Acceptable
Dip MP (W) (95% CI) [Interpretation]	0.95 (0.90 – 0.98) Excellent	8.55 (6.36 – 11.67) Acceptable	0.93 (0.86 – 0.97) Good	7.72 (5.25 – 10.29) Acceptable	0.75 (0.55 – 0.88) Moderate	10.52 (8.83 – 14.84) Unacceptable
Thrust MP (W) (95% CI) [Interpretation]	0.97 (0.95 – 0.99) Excellent	5.53 (3.54 – 7.26) Acceptable	0.98 (0.95 – 0.99) Excellent	5.53 (3.54 – 7.26) Acceptable	0.95 (0.89 – 0.98) Good	5.02 (4.85 – 7.39) Acceptable
Dip Imp (N.s) (95% CI) [Interpretation]	0.96 (0.91 – 0.98) Excellent	9.78 (7.43 – 13.43) Acceptable	0.95 (0.91 – 0.98) Excellent	6.42 (3.61 – 8.19) Acceptable	0.95 (0.89 – 0.98) Good	8.68 (4.81 – 11.04) Acceptable
Thrust Imp (N.s) (95% CI) [Interpretation]	0.98 (0.97 – 0.99) Excellent	4.32 (3.35 – 5.97) Acceptable	0.99 (0.98 – 1.00) Excellent	2.54 (1.05 – 3.06) Acceptable	0.95 (0.90 – 0.98) Good	3.44 (4.25 – 5.52) Acceptable

ICC intraclass correlation coefficient, CV coefficient of variation, CI confidence interval, PF peak force, MF mean force, PP peak power, MP mean power, Imp impulse

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307 The results of the one-way ANOVA demonstrated no significant or meaningful
308 differences for the thrust peak ($p = 0.84$) and mean force ($p = 0.87$) between the PP (2548
309 ± 512 N, 2295 ± 453 N, respectively), PJ (2646 ± 520 N, 2373 ± 462 N, respectively) and
310 SJ (2640 ± 528 N, 2368 ± 471 N, respectively) with small effect sizes ($\eta^2 < 0.008$). There
311 were no significant or meaningful differences for the thrust peak ($p = 0.83$) and mean
312 power ($p = 0.83$) between the PP (3136 ± 922 W, 1829 ± 475 W, respectively), PJ (3299
313 ± 987 W, 1934 ± 522 W, respectively) and SJ (3322 ± 904 W, 1906 ± 486 W, respectively)
314 with small effect sizes ($\eta^2 < 0.008$). No significant or meaningful differences ($p = 0.95$,
315 $\eta^2 = 0.002$) were found when comparing the thrust impulse between exercises (PP, 226 \pm
316 61 N.s; PJ, 233 ± 63 N.s; SJ, 232 ± 60 N.s) (**Figure 2**). Similarly, no significant or
317 meaningful differences were found when comparing the dip peak force (PP, 2325 ± 453
318 N; PJ, 2428 ± 475 N; SJ, 2424 ± 512 N; $p = 0.79$), dip mean force (PP, 1988 ± 445 N;
319 PJ, 2013 ± 416 N; SJ, 2017 ± 410 N; $p = 0.98$), dip peak power (PP, -1152 ± 420 W; PJ,
320 -1213 ± 415 W; SJ, -1199 ± 405 W; $p = 0.91$), dip mean power (PP, -840 ± 275 W; PJ, -
321 870 ± 282 W; SJ, -858 ± 271 W; $p = 0.95$) and dip impulse (PP, 99 ± 31 N.s; PJ, 100 \pm
322 31 N.s; SJ, 100 ± 33 N.s; $p = 0.99$) with small effect sizes ($\eta^2 \leq 0.01$).

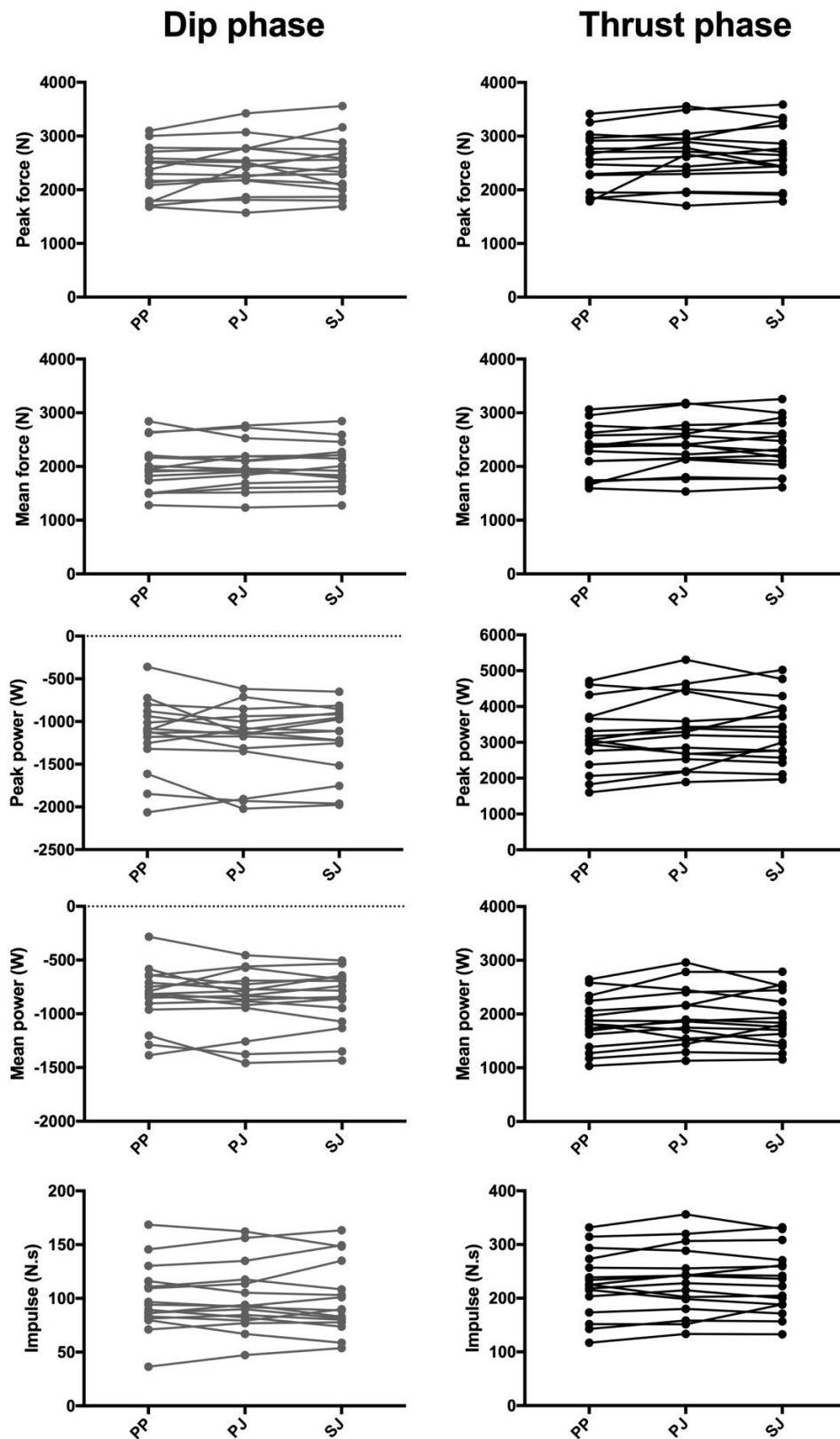


Figure 2. Kinetics recorded in the dip and thrust phases during the push press, push jerk and split jerk. Each circle represents the outcome of one participant in the three exercises. The thin line links the outcomes of the three exercises for each participant. There were no significant ($p > 0.05$) differences in kinetics between the push press, push jerk and split jerk ($p > 0.05$) with small effect sizes ($\eta^2 < 0.01$). *PP* push press, *PJ* push jerk, *SJ* split jerk.

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Table 2. Lifting strategy kinematics underpinning kinetic performance variables during the push press, push jerk and split jerk

Lifting strategy kinematics	PP (average)	PJ (average)	SJ (average)	<i>p</i> (η^2)
Dip displacement (m) [range]	0.20 ± 0.05 [0.10 – 0.28]	0.19 ± 0.04 [0.14 – 0.27]	0.20 ± 0.05 [0.13 – 0.27]	0.98 (0.001)
Thrust displacement (m) [range]	0.18 ± 0.05 [0.09 – 0.28]	0.19 ± 0.05 [0.10 – 0.28]	0.18 ± 0.04 [0.12 – 0.27]	0.92 (0.004)
Dip duration (s) [range]	0.53 ± 0.08 [0.38 – 0.66]	0.52 ± 0.11 [0.33 – 0.76]	0.51 ± 0.13 [0.32 – 0.82]	0.88 (0.006)
Thrust duration (s) [range]	0.23 ± 0.05 [0.14 – 0.34]	0.22 ± 0.05 [0.12 – 0.33]	0.22 ± 0.05 [0.14 – 0.34]	0.93 (0.003)

PP push press. *PJ* push jerk, *SJ* split jerk

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In addition, there were no significant or meaningful differences for the dip ($p = 0.98$) and thrust ($p = 0.92$) displacement of the PP (0.20 ± 0.05 m, 0.18 ± 0.05 m, respectively), PJ (0.19 ± 0.04 m, 0.19 ± 0.05 m, respectively) and SJ (0.20 ± 0.05 m, 0.18 ± 0.04 m, respectively) with small effect sizes ($\eta^2 < 0.01$). Similarly, there were no significant or meaningful differences when comparing the dip ($p = 0.87$) and thrust ($p = 0.93$) duration of the PP (0.53 ± 0.08 s, 0.23 ± 0.05 s, respectively), PJ (0.52 ± 0.11 s, 0.22 ± 0.05 s, respectively) and SJ (0.51 ± 0.13 s, 0.22 ± 0.05 s, respectively) with small effect sizes ($\eta^2 < 0.01$) (**Table 2**).

336

Discussion and implications

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The findings of this study should aid strength and conditioning coaches during selection of exercises for a structured and periodized training program. Briefly, the results of this study show no significant or meaningful differences in kinetics between the three weightlifting overhead pressing derivatives (PP, PJ and SJ) performed at a standardized load of 80% 1RM PP. As hypothesized, these findings may be due to the similarities in

342 the lower-body lifting strategy kinematics for all lifts. Additionally, the inter-repetition
343 reliability was moderate to excellent for all the variables analysed (**Table 1**). It is
344 important to note that although the reliability was questionable for some measures of the
345 dip kinetics (SJ peak power and mean power and PP peak power), the reliability for all
346 measures of the thrust (propulsion) kinetics during the three exercises was good to
347 excellent.

348 There were no differences in PP, PJ, and SJ peak and mean force. These results
349 are in line with Comfort et al. (Comfort et al., 2011a) who reported no differences
350 between the mid-thigh clean pull and mid-thigh power clean, when performed at a load
351 of 60% 1RM power clean. Similarly, there were no differences for the peak and mean
352 power output between the PP, PJ, and SJ (**Figure 2**), in line with previous results on the
353 kinetics of power clean variations when performed at a fixed load (Comfort et al., 2011b;
354 Suchomel et al., 2014). These lack of differences in kinetics could be explained by the
355 fact that there were no significant differences ($p > 0.88$) in the dip and thrust displacement
356 and time between the PP, PJ and SJ, suggesting that a similar technical execution of the
357 movement pattern may not affect the force-time characteristics and the resulting power
358 generating capacity of weightlifting overhead pressing derivatives.

359 Researchers recently reported differences in the 1RM performance between the
360 PP (87%), PJ (95%), and SJ (100%) due to the fact that the catch phase enables the lifter
361 to drop underneath the barbell during the PJ and SJ, which reduces the requisite vertical
362 barbell displacement needed to complete each lift (Soriano et al., 2019). In our study, the
363 differences in the subjects' 1RM performances (PP = 85%; PJ = 92%; SJ = 100%) were
364 in line with previous results, and a fixed load of 80% of the 1RM PP was selected for the
365 comparison of the three exercises, resulting in lower relative loads for the PJ (74%) and
366 SJ (68%). Therefore, it may be reasonable to expect differences in kinetics between the

367 three exercises because during the PP the lifter is required to accelerate the system mass
368 across the full range of motion, pressing and locking the barbell overhead without re-
369 flexing the hips, knees and ankles. In contrast, the PJ and SJ do not strictly require an
370 upper-body pressing motion through the entire barbell displacement and also allows the
371 lifter to drop underneath the barbell, where less impulse could be an efficient option to
372 catch the barbell overhead. However, in this study participants were specifically
373 instructed to perform each lift (PP, PJ, and SJ) with maximum effort (*'push the floor as*
374 *hard as possible'*) to maximize the force that could be applied to the system in the
375 relatively short contraction time that the lift demands, in line with standardized training
376 practices to maximise intent during exercise performance (Kawamori & Newton, 2006).
377 Then, these findings highlight that even when the load is fixed to a certain percentage of
378 one exercise (80% 1RM PP), practitioners could expect similar kinetics between the PP,
379 PJ and SJ as long as their athletes lift with maximum effort.

380 Weightlifting overhead pressing derivatives have been compared with exercises
381 with similar lower-body kinematics in previous research (Comfort, Mather, & Graham-
382 Smith, 2013; Comfort et al., 2016; Lake et al., 2014). Comfort et al. (2016) compared the
383 peak power output achieved during the squat jump, mid-thigh power clean and PP across
384 50, 60 and 70% 1RM in male amateur athletes. Researchers determined that there were
385 no significant differences ($p > 0.05$) between exercises in peak force, rate of force
386 development, and power performed with a standardized load of 60% 1RM power clean
387 (Comfort, et al., 2013). Similarly, Lake et al. (2014) demonstrated no significant
388 differences between PP and jump squat maximum peak power output (7% , $p = 0.08$),
389 impulse applied to the load that maximized peak power (8%, $p = 0.17$) and mean power
390 (13%, $p = 0.91$); however, PP maximum mean power output was significantly greater
391 than the jump squat ($\sim 9.5\%$, $p = 0.03$). Interestingly, Garhammer (1985; 1991) found

392 similarities between snatch and clean second pull power (3004 to 4904 W, 3723 to 6255
393 W, respectively) with the jerk (4033 to 6953 W), in experienced weightlifters. The lack
394 of significant or meaningful differences may be attributable to the fact that propulsion
395 phase kinematics were similar between exercises, as with this study, therefore resulting
396 in no differences in kinetics (i.e. force, impulse, power). Together, these findings support
397 the notion that weightlifting overhead pressing derivatives such as the PP may be a
398 suitable option to effectively develop rapid lower-body force and power generating
399 capacity. This is because the PP, PJ or SJ present similar lower-body mechanical demands
400 during the propulsion phase compared with other ballistic and weightlifting exercises
401 such as the jump squat, mid-thigh power clean and snatch (Comfort et al., 2013;
402 Garhammer, 1991; Garhammer, 1985).

403 To our knowledge, this is the first study aimed to compare the kinetics between
404 the main three weightlifting overhead pressing derivatives that could help strength and
405 conditioning coaches to select the most appropriate weightlifting variation for developing
406 lower-body strength and power. However, this study has several limitations that should
407 be addressed in future research. First, there were no highly skilled weightlifters in this
408 study; therefore, as the differences in weightlifting performance are affected by sport
409 group (Soriano et al., 2019), the results of this study should be extrapolated with caution
410 to weightlifters with a high technical proficiency. Second, it is essential to note that the
411 effect of load was removed from this study to focus on the influence of exercise selection
412 purely. Therefore, further research investigating the kinetics and lower-body lifting
413 strategy kinematics of these lifts employing a broader range of loads (i.e. 60, 70, 80, 90%
414 1RM PP) is guaranteed for comparisons of the PP, PJ, and SJ. Based on previous studies
415 focused on power clean variations, it may be hypothesized that lighter and heavier loads
416 would change the lifting strategy kinematics, and therefore, the resulting kinetics

417 (Comfort, Jones, & Udall, 2015; Comfort, Udall, & Jones, 2012). Third, in this study the
418 relative load was based on the PP 1RM performance for the comparison of the three
419 exercises, resulting in lower relative loads for the PJ (74%) and SJ (68%); considering
420 that heavier loads can hypothetically be lifted during the PJ and SJ, future research should
421 address the comparison of kinetics and lifting strategy kinematics between the PP, PJ and
422 SJ based using their respective relative loads. This will help strength and conditioning
423 coaches to make evidence-based decisions regarding exercise and load selection to
424 enhance the force-velocity relationship of their athletes (Suchomel, Lake, & Comfort,
425 2017).

426 **Conclusions**

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429 There were no significant or meaningful differences in kinetics between the main
430 weightlifting overhead pressing derivatives when performed at the same standardized
431 load of 80% 1RM PP. In addition, there was a moderate to excellent inter-repetition
432 reliability for the kinetics of the PP, PJ and SJ.

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560 **Figure captions**

561 **Figure 1.** Graphic representation of the force-time and the integrated velocity-time characteristics of the
562 push press exercise performed at 80% of 1RM by a random participant. Force is represented as the system
563 mass (force exerted by the participant plus barbell and body weight). *F* force, *v* velocity. **Dip** corresponds
564 to the unweighting and braking phases of the lift, with negative direction. **Thrust** corresponds to the
565 propulsion phase, with positive direction.

566

567 **Figure 2.** Kinetics recorded in the dip and thrust phases during the push press, push jerk and split jerk.
568 Each circle represents the outcome of one participant in the three exercises. The thin line links the outcomes
569 of the three exercises for each participant. There were no significant ($p > 0.05$) differences in kinetics
570 between the push press, push jerk and split jerk with small effect sizes ($\eta^2 < 0.01$). *PP* push press, *PJ* push
571 jerk, *SJ* split jerk.

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